

Environmental mineralization of caffeine micro-pollutant by Fe-MFI zeolites

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35	10	Key words: Fe-MFI; zeolite; caffeine; micro-pollutant; mineralization; Fenton reaction.
36	10	
37 38		
39	11	Abstract
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43	12	Environmentally emerging micro-pollutant, caffeine, was mineralized (i.e full degradation)
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45 46	13	by the isomorphic incorporation of Fe into silicalite-1 (MFI structure zeolite) through a
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48	14	microwave synthesis method. The Fe incorporation conferred mesopore formation that
49 50		
51	15	facilitated caffeine access and transport to the MFI zeolite structure. Increasing the Fe
52 52	16	content forward the formation of $\Gamma_{0}(\Omega)$, sites within the MEL structure. The actual tip estimate
53 54	16	content favored the formation of Fe(O) ₄ sites within the MFI structure. The catalytic activity
55	17	for the degradation of caffeine increased as a function of Fe(O)4 sites via a Fenton-like
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heterogeneous reaction, otherwise not attainable using Fe-free pure MFI zeolites.
Caffeine degradation reached 96% (TOC based) for zeolites containing 2.33% of Fe.

1. Introduction

Caffeine is rapidly becoming a contemporary anthropogenic pollutant in natural waters. It has been found in lakes in Switzerland (Buerge et al., 2003) and in the sea coast of Oregon (Rodriguez del Rey et al., 2012) in the USA. Caffeine pollution may be caused by effluents from our current lifestyle, related to drinking coffee and many energy drinks containing caffeine. Although the caffeine toxicity is of little concern for humans under moderate conditions, a similar generalization for aquatic organisms cannot be made since they are continuously exposed over a lifetime (Bruton et al., 2010). Hence, it is imperative to avoid future detrimental environmental impacts if caffeine continues to accumulate in natural waters. Caffeine can be degraded biochemically by Pseudomonas bacteria (Gummadi et al., 2009), by photolysis (Bruton et al., 2010), or by using chemical processes such as ozonation (Rosal et al., 2009). Advanced oxidation processes (AOPs) are also attractive in tackling caffeine degradation, particularly due to the simplicity of coupling catalysts and oxidants in a single unit operation. One of the most promising AOPs is the heterogeneous Fenton reaction using iron oxide catalyst and hydrogen peroxide (H₂O₂) oxidant (Klamerth et al., 2012, Zeng et al., 2015). In this reaction, the active sites (\equiv Fe²⁺) react with H₂O₂ and generate OH radical, a powerful oxidant extensively used in the degradation of organic compounds in wastewaters by AOPs processes (Zubir et al., 2015, Mijangos et a., 2006). The Fenton reaction approach was recently investigated for caffeine degradation using bio-based combined iron oxide photo

40 catalysts (Franzoso et al., 2017) and persulfated activated iron catalysts (S. Rodríguez
41 et al., 2017).

Zeolites are efficient materials for separation (Rangnekar et al., 2015), adsorption (Hoffmann et al., 1997) and catalysis (Vermeiren and Gilson, 2009 and Li et al., 2014) applications, though they are generally used as adsorbents in water and wastewater treatment (Kragovi et al., 2013, An, 2013 and Wingenfelder et al., 2005). They can be prepared and used as either purely microporous or hierarchical micro/mesoporous materials (Pérez-Ramírez et al., 2008). The latter form decreases diffusion restrictions and is widely applied in sorption (Meng et al., 2011) and catalysis (Christensen et al., 2003). A large variety of functionalities, such as acid-base or redox centers, can be introduced in zeolites (Moliner, 2012). Heteroatoms, such as Fe, can be incorporated in zeolites through various methods such as cationic exchange, impregnation, or chemical vapor deposition of metal precursors after zeolite crystallization (post-synthesis treatment). Another strategy, called "one pot", consists in the direct insertion of heteroatoms during zeolite formation (Bordiga et al., 1996, Giordano et al., 2002); and is an attractive option for lowering the manufacturing costs and ensuring uniform dispersion of heteroatoms in either framework or extra-framework positions.

In-situ hydrothermal synthesis methods have been used to provide isomorphic incorporation of Fe into MFI zeolite structure, although reports to date have limited the Si/Fe molar ratio to 100 (1 at%Fe) (Kritchayanon et al., 2006; Taniguchi et al., 2016). Further Fe incorporation can be carried out by post-synthesis methods, but they mostly yield extra-framework iron oxide species (Maxwell et al., 2003; Anizelli et al., 2016). The isomorphic incorporation of iron species into zeolites differs from conventional

63 immobilization of iron-based particles (e.g. Fe, Fe₂O₃ or Fe₃O₄) on substrates such as 64 graphene oxides (Zubir et al., 2014), silica shells (Liu et al, 2014), carbon aerogels (Wang 65 et al., 2013) or clays (Gao et al., 2015). The main advantage of inserting transition 66 elements in zeolites by direct synthesis is related to the possibility of achieving a high 67 dispersion of the metal in the zeolitic structure.

Herein, we show the production of higher Fe content Fe-MFI zeolites confers enhanced catalytic performance for the mineralization of caffeine as compared to traditional pure MFI zeolites. The as-synthesized Fe-MFI zeolites were tested for the catalytic caffeine removal from synthetic wastewaters under the conditions of the Fenton-like heterogeneous reaction. The catalytic testing was accompanied by the charactersition of Fe-MFI zeolites. Of particular interest, the catalytic results are corelated to the role played by Fe–O sites in the mesoporous zeolite structure, in order to provided new insights into the improved catalytic efficiency of Fe-MFI zeolites.

2. Experimental

2.1. Materials Synthesis

The zeolite synthesis solutions were prepared by mixing TEOS (98%, Aldrich), ultrapure water (18.2 M Ω), tetrapropyl ammonium hydroxide (TPAOH, 20 wt% aqueous solution, Sigma) and iron (III) acetylacetonate (Fe(acac)₃, 99.9%, Alfa Aesar). The sol molar concentration was set at (*x*/2) Fe₂O₃ :100 SiO₂ : 40 TPAOH : 1950 H₂O : 400 C₂H₅OH where *x* is the required atomic concentration of Fe in the MFI zeolite. Subsequently, the sols were aged under stirring for 24 h at 25 °C. The aged sols were placed into autoclaves in a commercial laboratory microwave oven (Milestone ETHOS 1600). The hydrothermal

treatment was conducted as one pot synthesis. Initially, the closed autoclaves were irradiated for 90 min at 80 °C with a MW power of 250 W. Subsequently, the autoclaves were heated to 180 °C and left for 60 min under MW irradiation of 400 W. Finally, the autoclaves were cooled down to 50 °C before opening. The formed solid products were separated by centrifugation at 9500 rpm (JOUAN B4i) and washed twice with distilled water. A centrifugation step followed after each wash. The washed solids were dried for 4 h at 155 °C prior to calcination. The dried materials were then calcined in air at 550 °C for 8 h with heating and cooling rates of 5 $^{\circ}$ C min⁻¹.

Characterization. A PANalytical X'Pert Pro X-ray diffractometer operating at 40 mA and 40 kV was used for measurement of X-ray diffraction patterns. PANalytical X'pert Pro software was used to determine the crystal phase and calculate the lattice constants. Morphological features of the samples were observed on a Hitachi S-4800 field emission scanning electron microscope (FESEM), and a JEOL JMS-2010 high resolution 36 100 transmission electron microscope (HR-TEM). The elemental composition of samples was assessed using a JEOL Model JSM-7001F SEM system equipped for energy-dispersive X-ray spectroscopy (EDS). X-ray spectra were collected with a JEOL Minicup EDS detector (Model EX-64175JMH), with a 133 eV resolution, 10 mm² effective area, polymer ultrathin window (UTW) and using JEOL Analysis Station JED-2300 Series (v. 3.84) 48 105 software. Microanalysis acquisition conditions were 20 keV at 10 mm working distance.

The descriptors (x%Fe-MFI) for the samples are based on the Fe content detected in the solid ascertained by EDS, where *x* represents the atomic percentage of Fe in (Si+Fe) mixture within the zeolite sample (i.e. x=0.34 (0.34%Fe-MFI)). A Renishaw inVia confocal Raman Microscope Spectrometer operated with UV laser line (325 nm) was employed

for Raman measurements. The Raman spectra were deconvoluted using Origin 8.5 software. Nitrogen sorption measurements were performed on a Micromeritics TriStar 3020 analyzer after degassing at 300 °C for 24 h under vacuum on a VacPrep061 degassing system. Specific surface area values were calculated by Brunauer-Emmett-Teller (BET) model, from adsorption data in the 0.05–0.20 relative pressure range (p/p₀). Pore diameters were determined via the density functional theory (DFT) modeling of the entire adsorption branch (p/p₀= 0.0005–0.95) using a cylindrical pore model on metal oxide surface with a regularization factor of 0.40. The minimum size modeled by DFT (12Å) was limited by the lower limit value of the relative pressure (p/p₀ ~5 x 10⁻⁴).

2.2. Catalysis experiments

The catalytic activity of materials was tested using 0.33 g L⁻¹ zeolite and a commercial Fe₃O₄ (98%, Sigma-Aldrich), deionized water at pH of 3 (adjusted by HCl, 36%wt, Chemsupply Pty Ltd) and 22 mM hydrogen peroxide (H₂O₂, 30%, Chem-supply Pty Ltd.). The caffeine concentration was varied from 10 to 20 and 50 ppm in solution at 25 °C. The oxidative degradation of caffeine was carried out using a fresh catalyst for each test. Liquid samples were taken after 1 h of dark adsorption, and 1, 3, 7 and 22 h after H_2O_2 was added. The concentration of caffeine in the solution was determined by measuring the absorbance of the filtered solution at 484 nm on an Evolution 220 UV-Vis spectrophotometer (Thermo Fisher Sci.). Experimental variation for the concentration of caffeine in the solution was ± 0.8 ppm. Total organic carbon (TOC) analysis was undertaken on a Shimadzu TOC analyzer with an Agilent Eclipse XDB-C8 4.6 x 150 mm column with 5 µm packing. The TOC analysis was carried out on a 150 µL sample, and

the organic carbon content was an average value calculated from four measurements for each tested catalyst and tested condition.

3. Results and discussion

The incorporation of Fe in MFI zeolites was carried out during zeolite formation, by a two-steps microwave-assisted hydrothermal synthesis method. Fe-MFI was produced from solutions with Si/Fe atomic ratios equal to ∞ (0 %Fe), 400 (0.25 %Fe), 200 (0.5 %Fe), 100 (1 %Fe) and 50 (2 %Fe), though the 25 (4%Fe) samples failed due to direct gelation of the sol. The Fe concentration in the produced powders, determined by EDS, generally showed a good transfer of Fe ions from the sol (0.25, 0.5, 1 and 2%) to the synthesized bulk materials resulting in measured Fe concentrations of 0.34, 0.66, 1.20 and 2.33 % in the solids, respectively. A wide angle XRD analysis was also conducted as displayed in Fig. 1 in order to determine the crystal structure of the materials. The measured patterns were compared to the reported in a PDF2 data basis and were attributed to reference pattern 01-070-4744. These XRD patterns confirm that all formed materials hold the monoclinic crystal structure (#14, P21/n1), characteristic for calcined MFI structure.

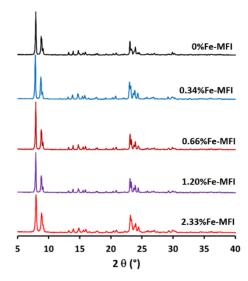


Fig. 1 XRD patterns of pure MFI (silicalite-1) and Fe-MFI powders (FeS-1) series calcined 7 at 550 °C. Table 1 lists the lattice parameters (a, b, and c) calculated from XRD patterns. As 10 151 15 153

expected for an isomorphous substitution of Si by Fe, the unit cell volume increased when 0.25% Fe was incorporated into the synthesis solution as compared with the blank 0%Fe-MFI sample. However, the cell volume values did not correlate with the quantity of Fe 20 155 detected by EDS. Rather, the unit cell volume peaked as x increased from 0 to 0.34%, before decreasing sequentially for higher Fe content. The β parameter, which is related 25 157 to the crystal lattice distortion, evolved by a different profile to the unit cell volume, peaking at Fe concentration of 1.20%. Interestingly, no secondary iron oxide phase was detected in the XRD patterns, thus confirming the presence of monoclinic crystal structure (#14, 32 160 P21/n1) (Treacy and Higgins, 2001). It is noteworthy that Fe-MFI zeolites were synthesized with Fe concentration in excess of 1% (i.e. Si/Fe < 100).

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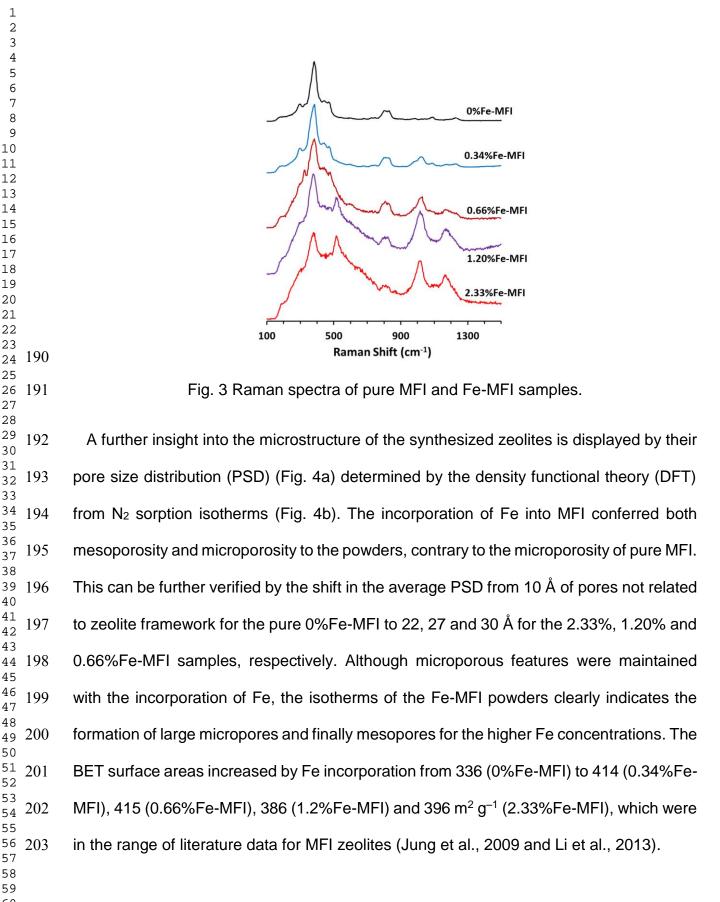
Table 1. Fe concentration in both sols and derived solids, and lattice constants of the corresponding MFI zeolites. x was measured by EDS. (atom %)

x%Fe-MFI sample										
sol	0	0.25	0.50	1.00	2.00					
solid (x)	0	0.34	0.66	1.20	2.33					
a (Å)	20.056 (5)	20.030 (4)	20.250 (1)	20.110 (3)	19.970 (1)					
b (Å)	19.990 (5)	20.069 (5)	20.158 (8)	20.140 (3)	20.100 (1)					
c (Å)	13.401 (3)	13.396 (4)	11.197 (5)	11.140 (2)	11.045 (8)					
α, β (°)	90, 90	90, 90	90, 90	90, 90	90, 90					

1 2 3 4 5		γ (°)	89.922 (3)	90.124 (4)	90.266 (7)	90.900 (3)	90.420 (1)
5 6 7		Vol. (ų)		5385	4571	4511	4433
8 9	165						
10 11 12			(a)		(b)		
$\begin{array}{c} 11\\ 12\\ 13\\ 14\\ 15\\ 16\\ 17\\ 18\\ 19\\ 20\\ 21\\ 22\\ 23\\ 24\\ 25\\ 26\\ 27\\ 28\\ 29\\ 30\\ 31\\ 32\\ 33\\ 34\\ 35\\ 36\\ 37\\ 38\\ 39\\ 40\\ \end{array}$			(a) 0 %Fe-MFI 200 nm 0.34%Fe-MFI 200 nm 0.66%Fe-MFI 200 nm 1.2%Fe-MFI			20 mm	
41 42 43 44 45 46 47 48 49 50 51 52 53 54 55	166 167	Fig. 2 (a) SEM a	2 <u>00 nm</u> 2.33%Fe-MFI 2 <u>00 nm</u>	HR-TEM inset		20 nm 20 nm 20 nm	nd Fe-MFI
55 56 57					mayes or pur	יזורו (ס-ו) נ נורו פון	
58 59 60 61 62 63 64 65	168	(FeS-1) powders	series.				9

The FE-SEM images in Fig. 2a clearly show that the MFI zeolite morphology was influenced by the Fe concentration. For instance, by raising the Fe concentration from 0 to 1.20%, the particles were getting rounder every time the Fe concentration was increased. Further increase of x from 1.20% Fe to 2.33% Fe yielded a packed and aggregated structure, resembling a cauliflower, comprised of smaller cubic crystals (< 100 nm). TEM images in Fig. 2b confirmed the formation of single crystal particles in samples derived from sols with the lowest iron concentrations (0 to 1.20% Fe). They are common features of MFI type zeolite morphology. Further increase of the Fe content at 2.33% resulted in a more complex polycrystalline structure made of aggregated cubic nanocrystals 40 nm in size.

To shed further light on Fe-MFI formation, Raman spectroscopy analysis was carried out to understand the incorporation of Fe ions. Fig. 3 shows two bands common to all samples (with and without Fe) at 378 cm⁻¹. The band at 378 cm⁻¹ is associated to with the Si–O–Si vibrations. The bands at 1165, 1019 and 516 cm⁻¹ were common to the iron-containing samples only. The bands at 1165 and 1019 cm⁻¹ were assigned to vibrational bands of Si-O-Si near iron and Fe-O-Si, respectively, and the 516 cm⁻¹ band was assigned to Fe(O)₄ in the zeolite network (Fan et al., 2009). Any additional bands potentially allocated to iron oxide particles (li et al., 2012) could not be observed at given conditions. Coupled with the absence of nano-particle domains in the HR-TEM images in Fig. 2b, these results clearly indicate that Fe was mainly incorporated in MFI particles as intra-framework species rather than as iron oxide (i.e. extra-framework) particles.



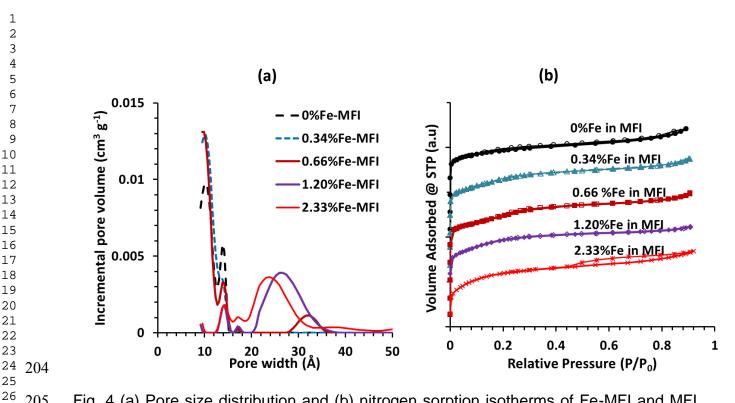


Fig. 4 (a) Pore size distribution and (b) nitrogen sorption isotherms of Fe-MFI and MFI samples.

32 207 The as-synthesized Fe-MFI samples were used as catalysts in a Fenton-like heterogeneous reaction as described in the experimental section. Fig. 5a clearly shows that the blank sample (%Fe-MFI) was unable to breakdown caffeine within 7 hours reaction, and only minor degradation was observed by 22 hours. Similar trends were also observed for the 0.34% and 0.66%Fe-MFI samples, which gave very low caffeine degradation rates. However, the results in Fig. 5a strongly suggest that the Fe has to be above a certain concentration to be effective in catalysis, in this case at least 1.20% Fe within the MFI powder. For comparison purpose, a commercially available Fenton like catalyst Fe₃O₄ was also tested for the degradation of caffeine reaching. The results in Fig. 5a confirm that the Fe-MFI zeolite catalysts were more efficient than the Fe₃O₄ catalyst. For instance, caffeine degradation of up to 98% and 90% were achieved by the 2.33%

and 1.23% Fe-MFI at 20 h, respectively, whilst the Fe₃O₄ catalyst reached a maximum degradation of 82%.

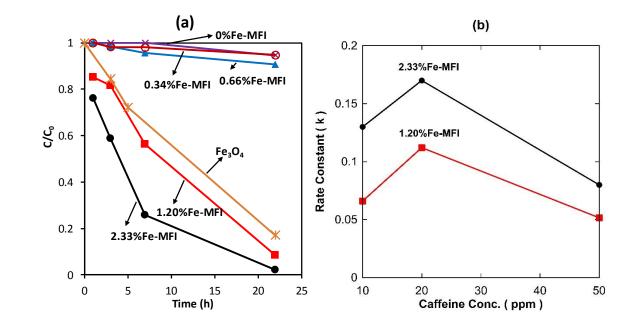


Fig. 5 (a) Caffeine degradation at concentration of 10 ppm in aqueous solution, and (b) rate constant at 10, 20 and 50 ppm @ 7 hours. All experimental conditions: H₂O₂=22 mM, pH=3 and 25 °C.

Fig. 5b displays the rate constant (k) for the same experimental work by varying the initial concentration of caffeine from 10 to 50 ppm for the most active samples (2.33%) and 1.20%Fe-MFI). Again these results demonstrate that the k values were greater for higher Fe content in the zeolite structure (2.33%Fe-MFI). The k value consistently 46 227 increased from 10 to 20 ppm, and then reduced when caffeine concentration increased further to 50 ppm. The reduction of the k value is associated with mass transfer limitations as adsorption was found to be negligible (\sim 1%). Further, as the surface area of the Fe containing MFI samples were very similar, the higher k values of 2.33%Fe-MFI were 58 232 therefore related to the amount of incorporated Fe.

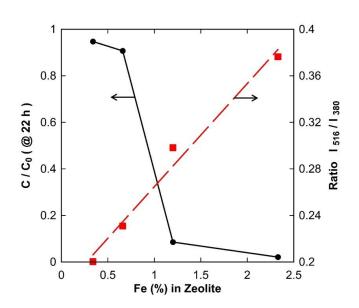


Fig. 6 Caffeine degradation and ratio of Raman peak areas at 516 and 378 cm⁻¹ as the function of iron fraction in Fe-MFI zeolite powders.

In order to explain the improved performance of Fe-MFI samples, the Raman spectra in Fig. 3 were deconvoluted to calculate the ratio of peak areas assigned to vibrational bands of the intra-framework species containing iron oxygen bonds (Fe(O)₄) at 516 cm⁻¹ over the MFI building units band at 378 cm⁻¹. Fig. 6 shows that the I₅₁₆/I₃₇₈ ratio increased almost linearly with an increase of iron content, showing good R² fitting correlations (0.982). This fitting confirmed the linearity within the Fe-MFI range in this work and the validity of the Raman deconvolution proposed by Fan and co-workers (Fan et al., 2010). In conjunction with the catalyst activity in Fig. 4a, the results in Fig. 6 strongly suggest that there is significant correlation between the presence of Fe(O)₄ sites and enhanced degradation of caffeine for Fe concentrations higher than 1.20% in the zeolite. The $Fe(O)_4$ sites are thus active in a Fenton-like process. This was accompanied by the presence of mesopores (20<d<35 Å) in the 1.20% and 2.33%Fe-MFI samples which favored the

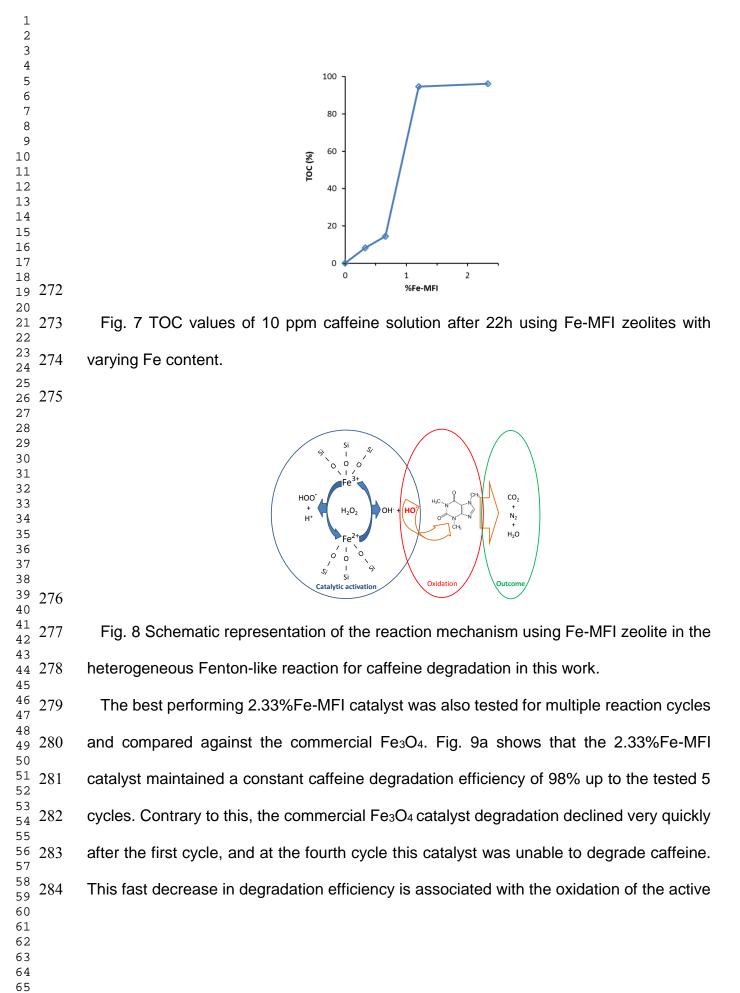
 diffusion of the small caffeine molecules (length: 10 Å) (Banerjee et al., 2012) into the
zeolite structure. The very low catalytic activity of the other Fe-MFI samples was attributed
to both insufficient Fe concentration, below 1.20% Fe, and microporosity leading to mass
transfer limitations.

Due to the large surface areas of the Fe-MFI powders (~380–390 m² g⁻¹), solid-liquid interface reactions occurred preferentially at the Fe(O)₄ sites. This reaction is schematically shown in Fig. 8 as isomorphic Fe(O)₄ sites embedded into the zeolite structure degrade caffeine. In this reaction, H₂O₂ was catalytically decomposed at the Fe²⁺ active sites into 'OH radicals and OH⁻ hydroxyl ions (Eq. 1). As proposed by Gonzalez-Olmos and co-workers (Gonzalez-Olmos, 2011), Fe²⁺ active sites are generated by the reaction of H_2O_2 with isolated Fe^{3+} sites at the Fe-MFI surface or by OOH radicals formed previously in the reaction of H_2O_2 with Fe³⁺ (Eq. 2). As confirmed by TOC analysis (Fig. 7), the powerful OH radicals mineralized the caffeine (C₈H₁₀N₄O₂) into CO₂, H₂O and N₂ species (Eq. 3). TOC analysis also confirms the degradation ratio ascertained by UV-vis measurement (Fig. 6), showing very high level of mineralization of caffeine at 94.5 and 96.0% for the 1.20% and 2.33% Fe-MFI samples, respectively. Therefore, this reaction is characterized by the reduction of Fe³⁺ to Fe²⁺ and oxidation of Fe²⁺ to Fe³⁺, concomitantly with the mineralization of caffeine. Provided H₂O₂ is supplied, these results demonstrate the potential of Fe-MFI zeolites to treat waters contaminated with caffeine micro-pollutants.

$$\equiv Fe^{2+} + H_2O_2 \rightarrow \equiv Fe^{3+} + OH + OH^-$$
(1)

$$\equiv Fe^{3+} + H_2O_2 \rightarrow \equiv Fe^{2+} + HOO^{\bullet} + H^+$$
(2)

$$1 \qquad C_8 H_{10} N_4 O_2 + 14^{\bullet} OH - 14 OH^- \rightarrow 8 CO_2 + 14 H_2 O + 2N_2 \tag{3}$$



phase Fe²⁺ into a non-acitve phase Fe³⁺ in Fe₃O₄ based catalysts (Zubir et al., 2015). In the case of the Fe-MFI catalyst, the multiple cycling stability strongly suggests that the active phase was maintained. This is confirmed by the Raman analysis (Fig.9b) which shows that the spectrum of the fresh sample remained unaltered after 5 cycles of caffeine degradation, thus confirming the catalytic stability of Fe-MFI upon cycling.

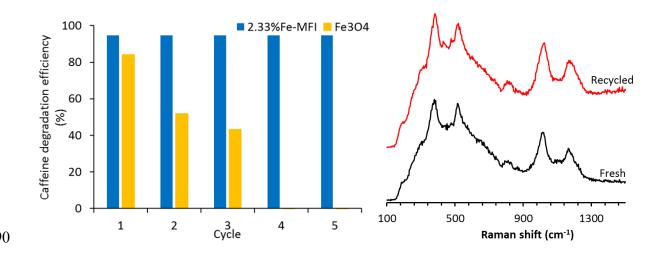


Fig. 9 (a) Cycling experiment conducted on 2.33%Fe-MFI zeolites and commercial Fe_3O_4 in a caffeine degradation ($C_{affeine} = 10$ ppm) at 20 h per cycle; (b) Raman spectra of fresh and a sample 2.33%Fe-MFI zeolite exposed to 5 cycles of caffeine degradation.

4. Conclusions

The incorporation of Fe with concentrations above 1.0% conferred mesoporosity to the Fe-MFI, thus facilitating the access of caffeine to the zeolite porous structure. The Fe(O)₄ bonds in the Fe-MFI zeolite structure were very active leading to the decomposition of H₂O₂ into radicals, thus promoting the degradation of caffeine in the heterogeneous Fenton-like reaction. The significant increase in catalytic activity was attributed to

mesoporosity coupled with Fe concentrations at and above 1.20% in the MFI structure.
TOC removal of 96% with 2.33%Fe-MFI sample was achieved.

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